

Development of scheme for solving fluid-structure problem based on loosely coupling method

疎結合計算をベースとした流体固体の連成解析の手法開発

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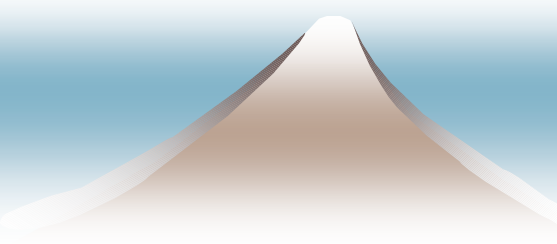
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Purpose

Development of the scheme for solving a fluid-structure problem on biomechanics

Future

To simulate the interaction between blood wall and blood



Main scheme of fluid-structure coupling problem

- ◆ **Loosely coupling method**

Fluid dynamics analysis with FDM \longrightarrow Structure analysis with dynamic FEM
analysis with FDM \longleftarrow with dynamic FEM

- ◆ **Direct coupling method**

CIP method(Cubic-Interpolated Polynomial)

ALE method(Arbitrary Lagrangian Eulerian)

Basic equations of fluid dynamics

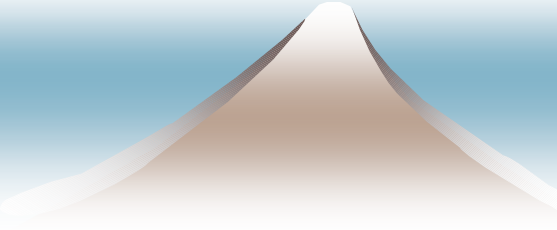
Navier-stokes equations

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} - \mathbf{u}_0) \nabla \mathbf{u} = -\nabla p + \frac{1}{\text{Re}} \nabla^2 \mathbf{u}$$

Continuity equations

$$\nabla \mathbf{u} = 0$$

Discretization with FDM

- 1 . **A third-order upwind** in convective term
 - 2 . **A second-order central scheme** in other spatial term
 - 3 . **A first-order Euler explicit** scheme for time integrations terms
 - 4 . **MAC method** is used to couple velocity and pressure field.
- 

Basic equations of elastic body(1)

Kinematic equations

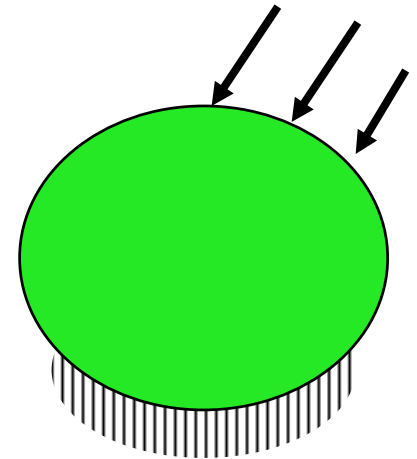
$$\sigma_{ij,j} = \rho \ddot{q}_i$$

Geometric boundary conditions

$$q_i = \bar{q}_i$$

Dynamic boundary conditions

$$\sigma_{ij} n_j = \bar{p}_i$$



Basic equations of elastic body(2)

Discretization with dynamic FEM

$$\mathbf{M}\ddot{\mathbf{q}} + \mathbf{C}\dot{\mathbf{q}} + \mathbf{K}\mathbf{q} = \mathbf{F}$$

Damping matrix

$$\mathbf{C} = \alpha\mathbf{M} + \gamma\mathbf{K}$$

Direct time integral method

Newmark β method

Acceleration

$$\ddot{\mathbf{q}}(t + \Delta t) = \left\{ \mathbf{M} + \frac{\Delta t}{2} \mathbf{C} + \beta \Delta t^2 \mathbf{K} \right\}^{-1} \\ \bullet \left[\mathbf{f}(t + \Delta t) - \left\{ \dot{\mathbf{q}}(t) + \frac{\Delta t}{2} \ddot{\mathbf{q}}(t) \right\} \right. \\ \left. - \mathbf{K} \left\{ \mathbf{q}(t) + \Delta t \dot{\mathbf{q}}(t) + \left(\frac{1}{2} - \beta \right) \Delta t^2 \ddot{\mathbf{q}}(t) \right\} \right]$$

Velocity

$$\dot{\mathbf{q}}(t + \Delta t) = \dot{\mathbf{q}}(t) + \frac{\Delta t}{2} \{ \ddot{\mathbf{q}}(t) + \ddot{\mathbf{q}}(t + \Delta t) \}$$

Displacement

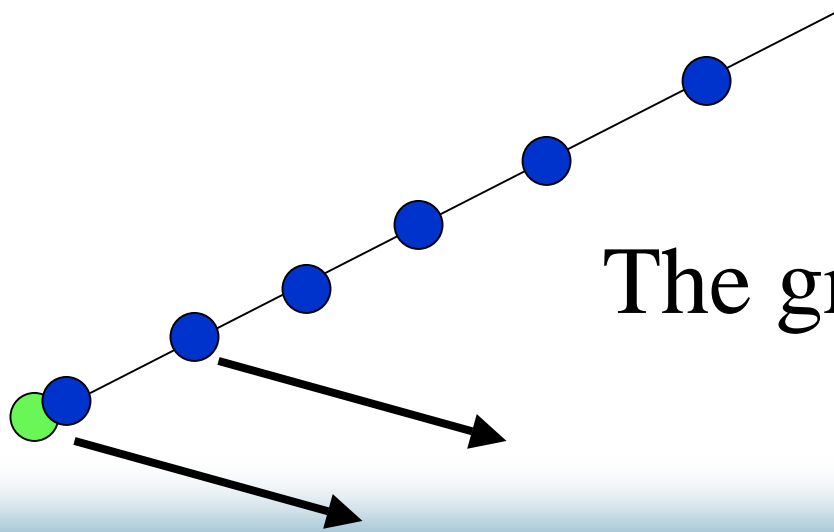
$$\mathbf{q}(t + \Delta t) = \mathbf{q}(t) + \frac{\Delta t}{1!} \dot{\mathbf{q}}(t) + \frac{\Delta t^2}{2!} \ddot{\mathbf{q}}(t) \\ + \beta \Delta t^3 \frac{\ddot{\mathbf{q}}(t + \Delta t) - \ddot{\mathbf{q}}(t)}{\Delta t}$$

The Velocity of moving grid

$$u_0 = \frac{x^{n+1} - x^n}{\Delta t}$$

$$v_0 = \frac{y^{n+1} - y^n}{\Delta t}$$

The
nodes of
FEM



The grids of FDM

Flow chart of scheme

Calculate stiffness matrix

Calculate mass matrix

Calculate damping matrix

Calculate coefficient matrix

Solve poisson equations

FDM

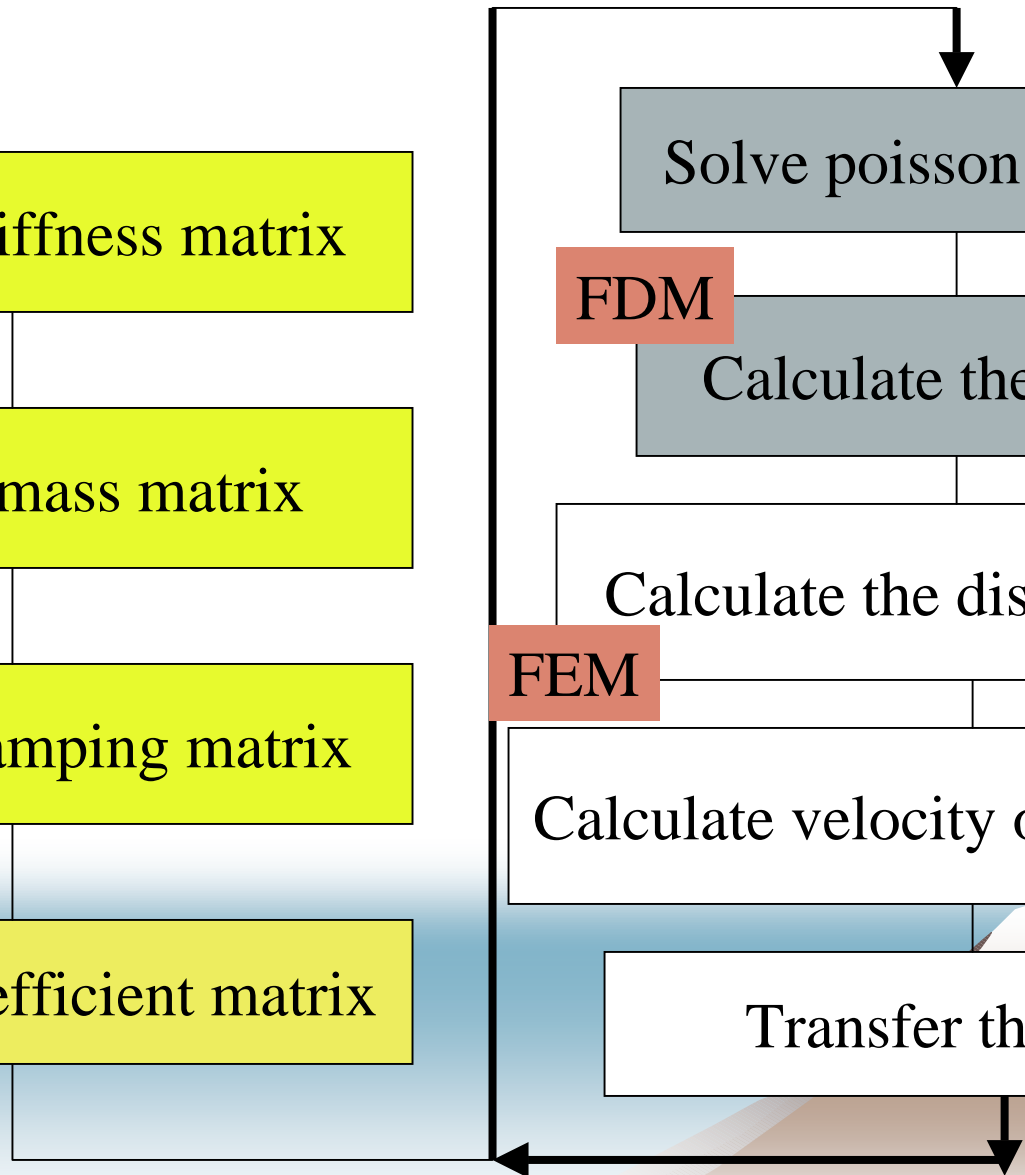
Calculate the velocity

Calculate the displacement

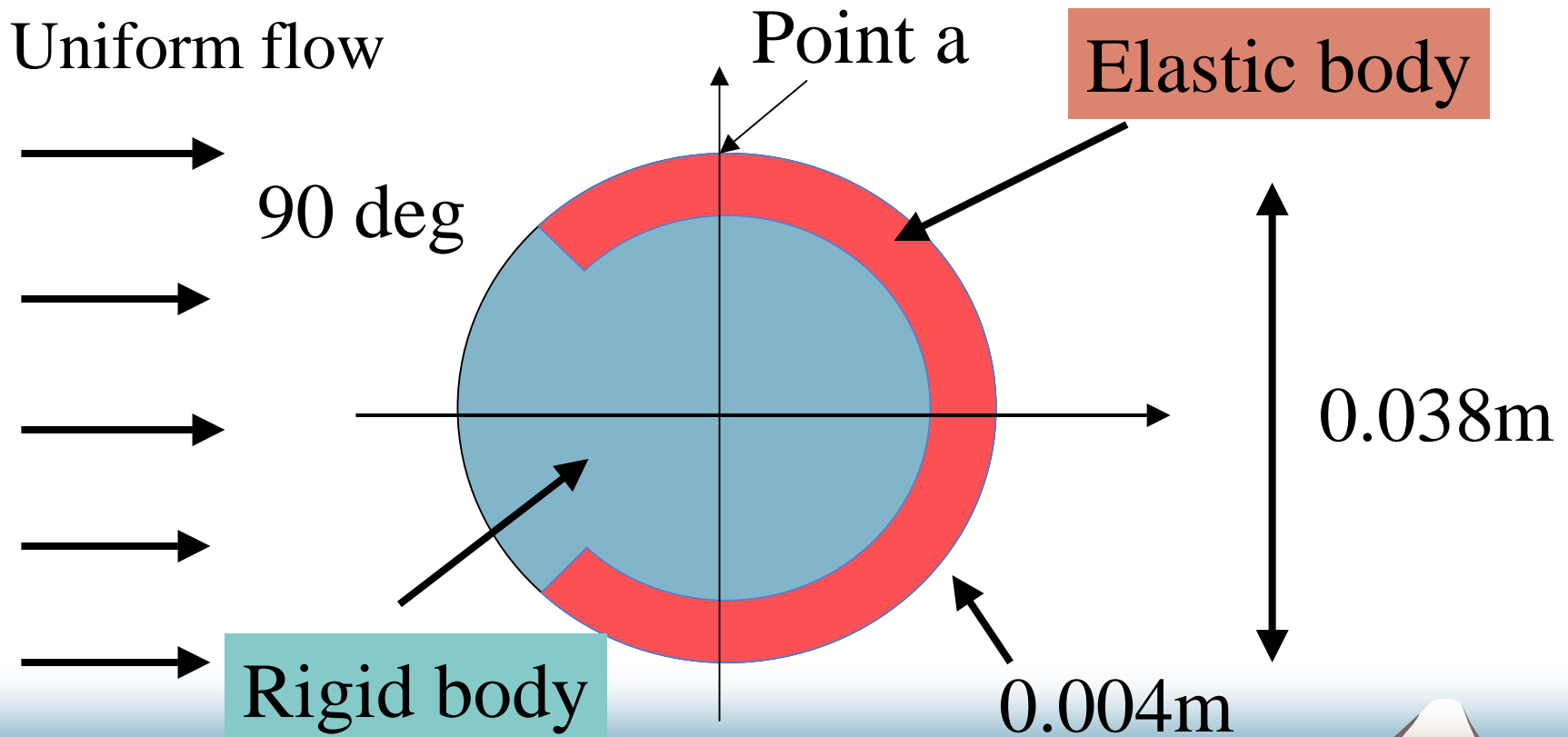
FEM

Calculate velocity of moving grid

Transfer the grids



Model of simulation



Calculation conditions

Fluid analysis

Reynolds number 10,000

$$\Delta t = 10^{-5}$$

Newmark
method

$$\beta = 0.25$$

Elastic analysis

Poisson's ratio 0.4

Young 's modulus
11,000[Pa]

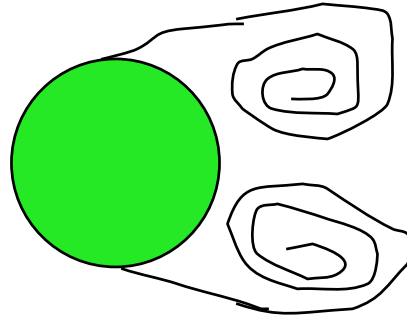
Damping matrix
coefficient

$$\alpha = 0.02 \quad \gamma = 0.05$$

Non dimensional time

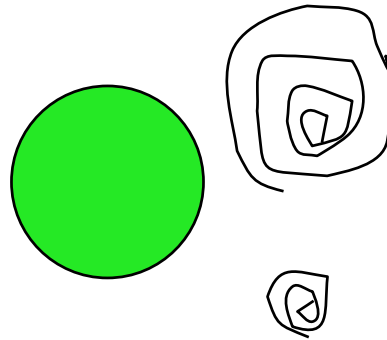
$T = 20.0$ (case 1), 60.0 (case 2),
 80.0 (case 3)

Case 1



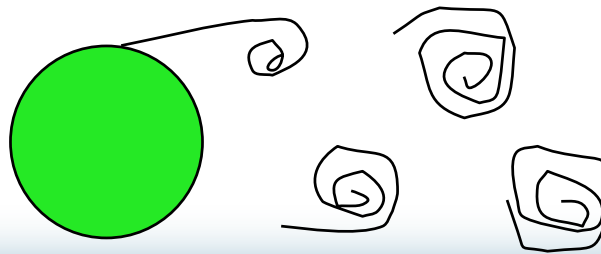
A pair of vortices

Case 2



Pre karman vortex
row

Case 3

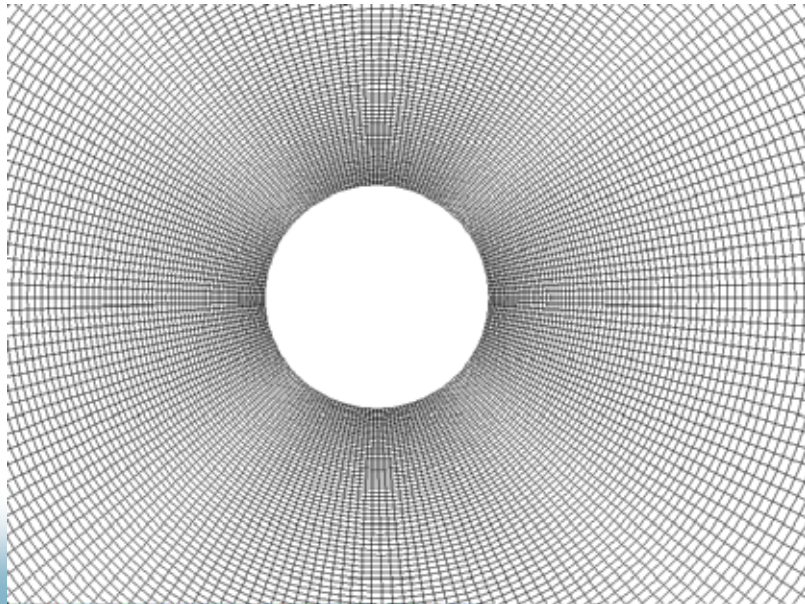


Karman vortex
row

Division of domains for fluid and elastic body

The number of grids

182×182

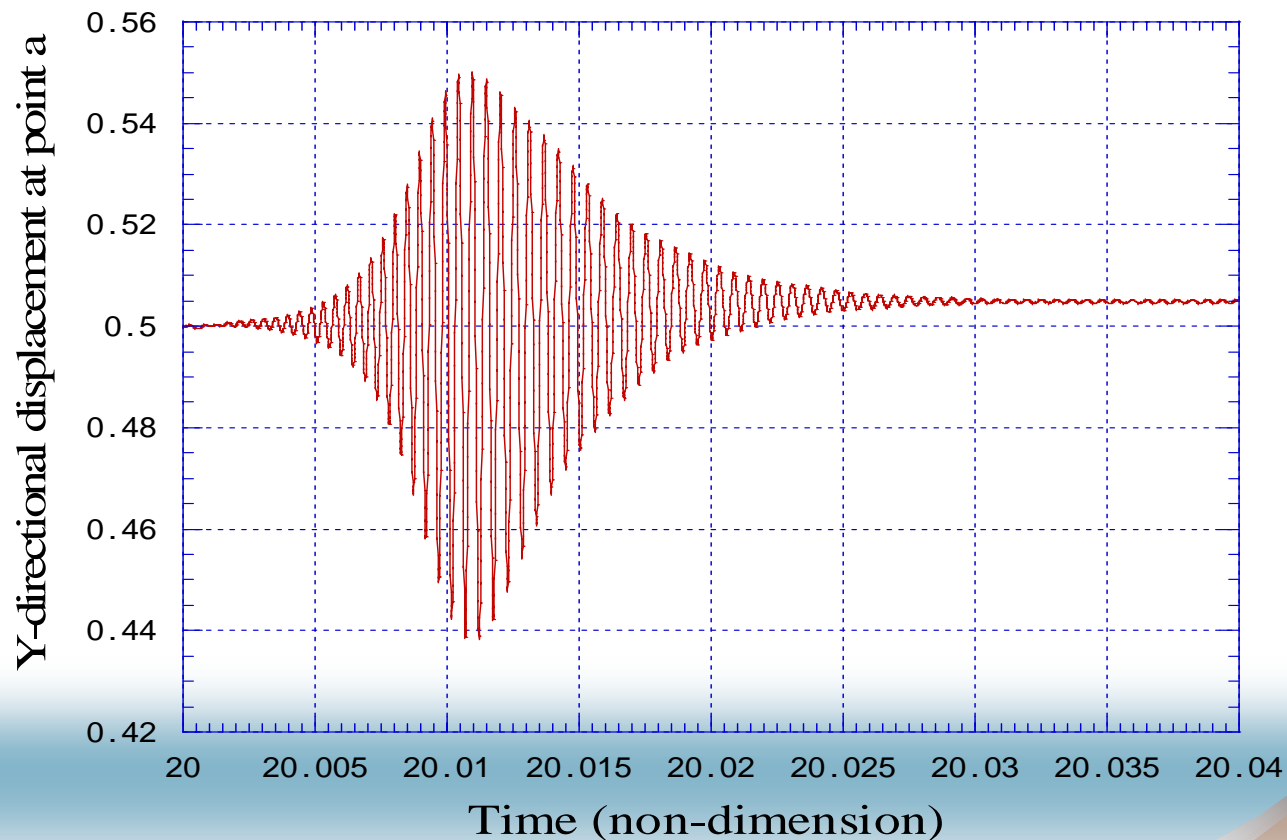


Triangular elements

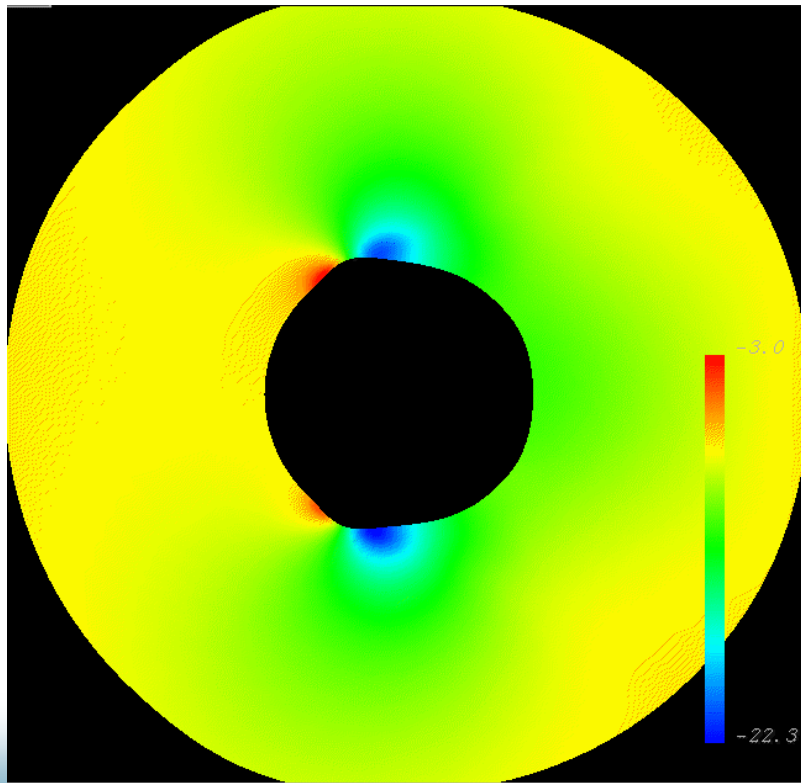
272 elements

One-dimensional interpolation function for displacement

The amplitude at point a in case 1

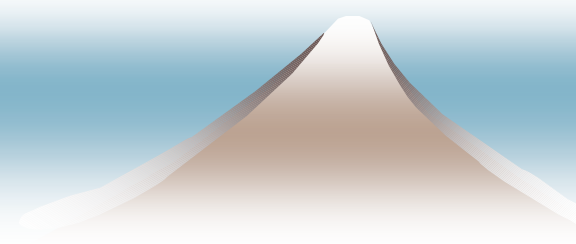
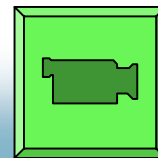
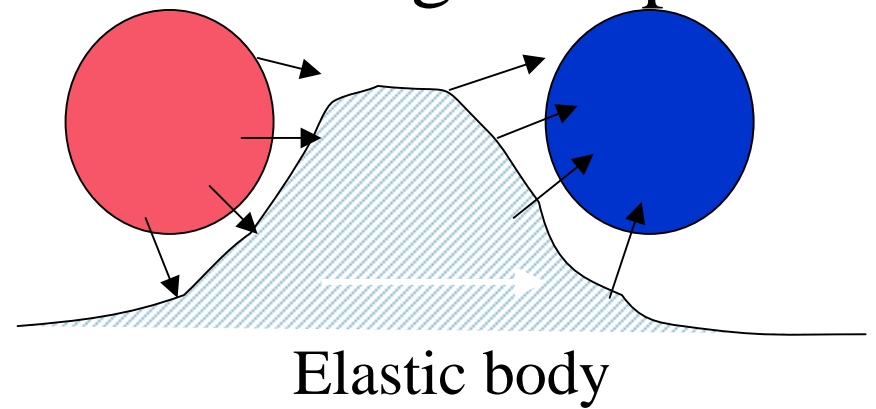


Generation of traveling wave

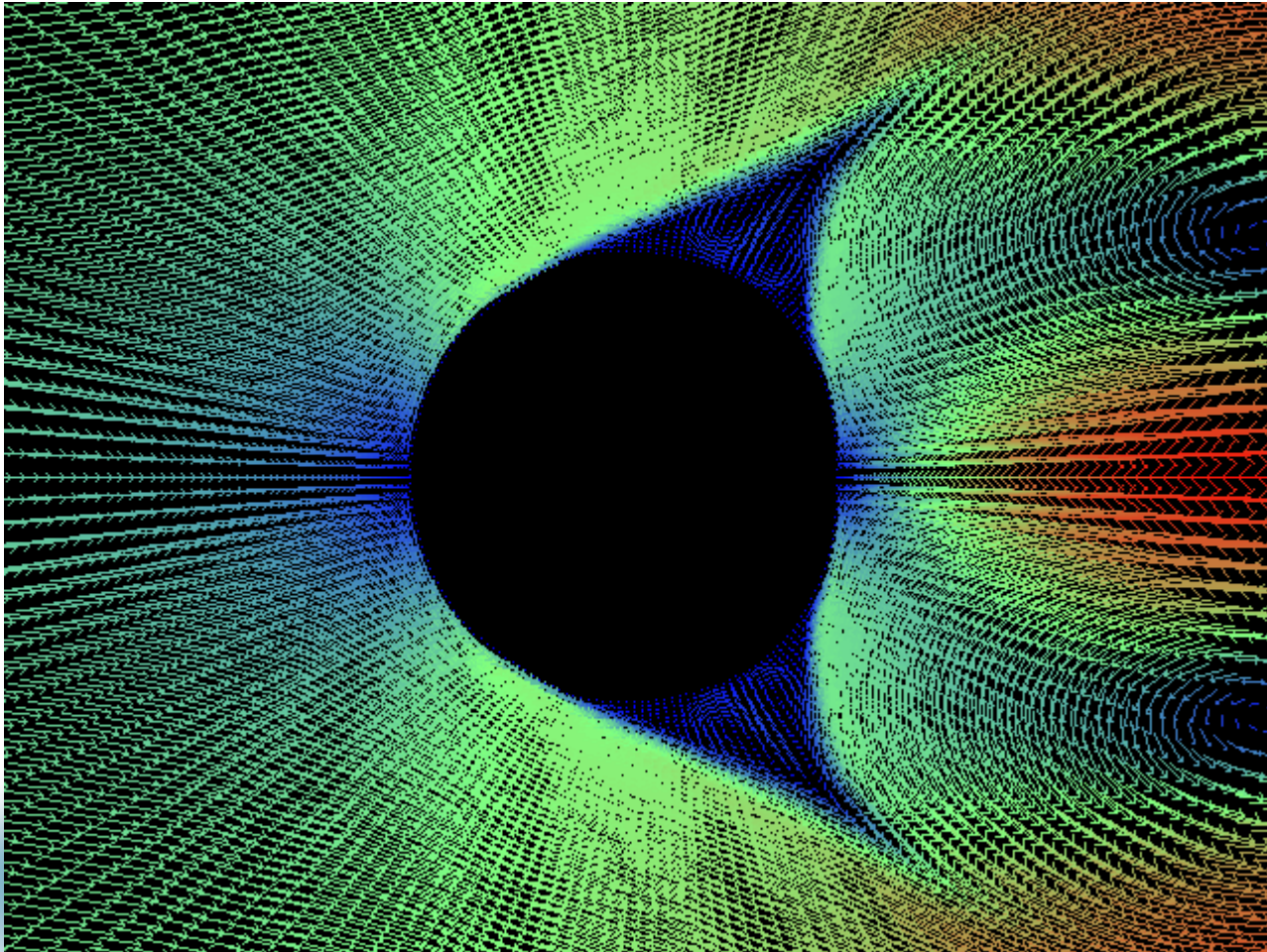


Positive pressure

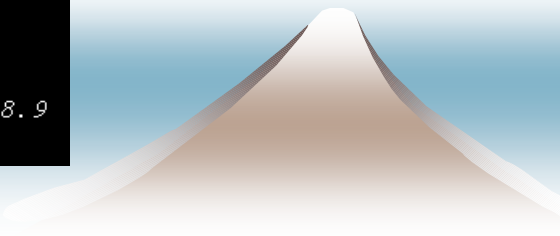
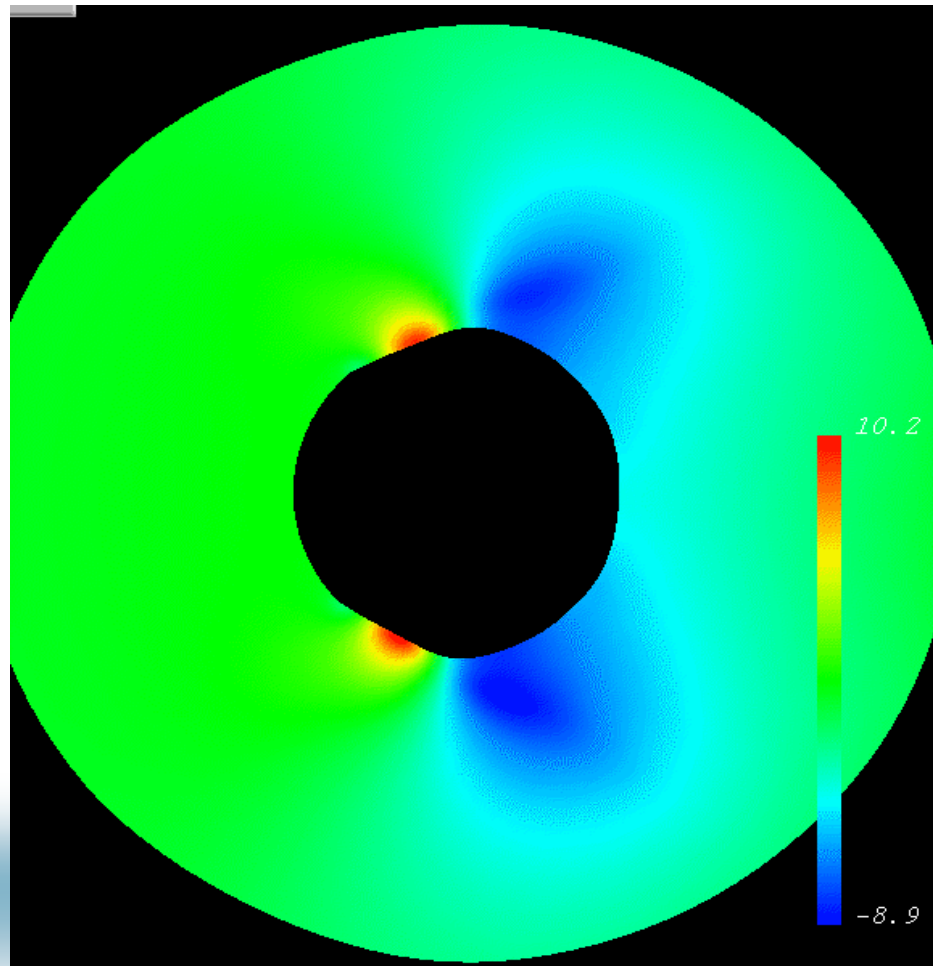
Negative pressure



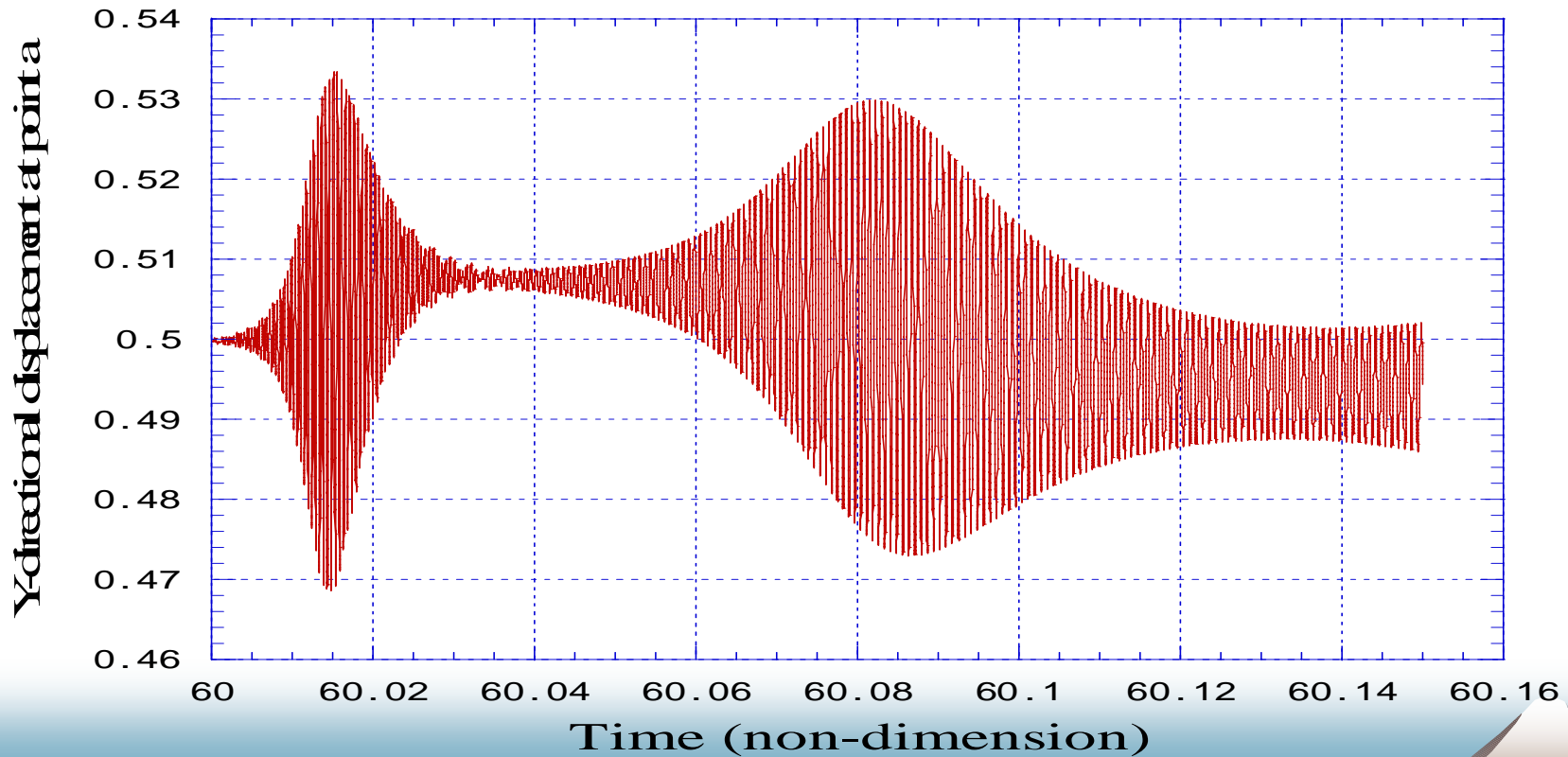
Vector line of velocity in case 1



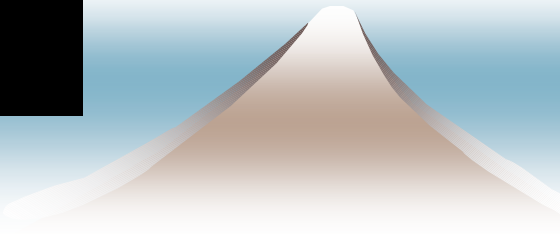
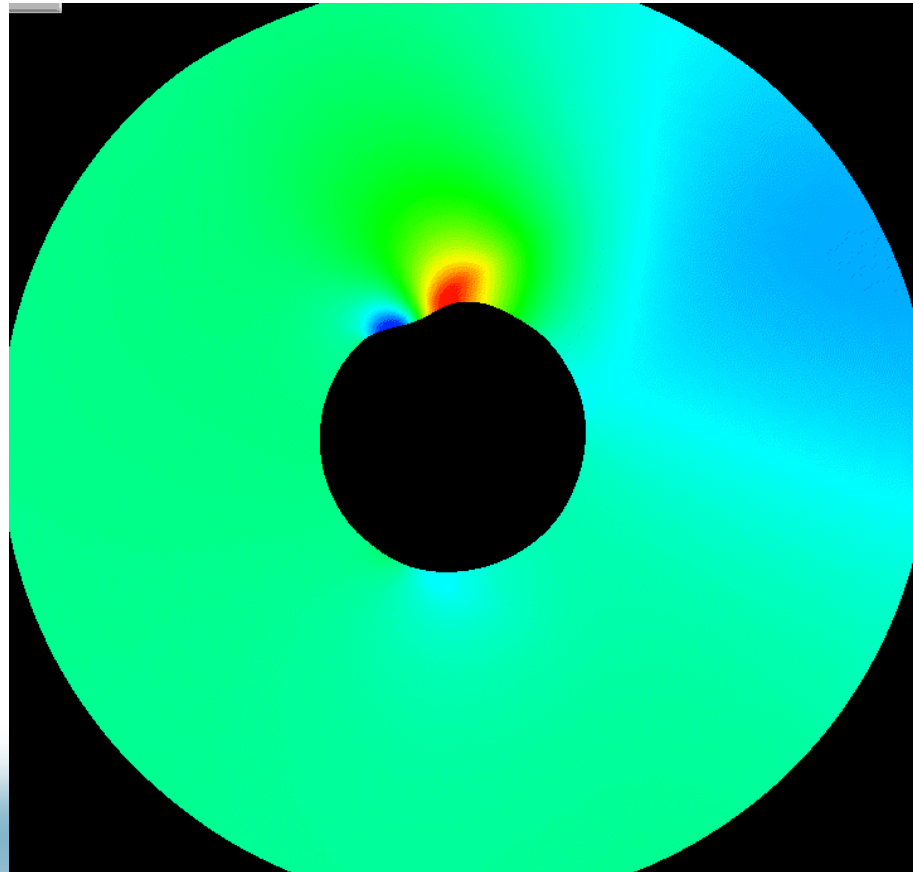
Deformation in case 1



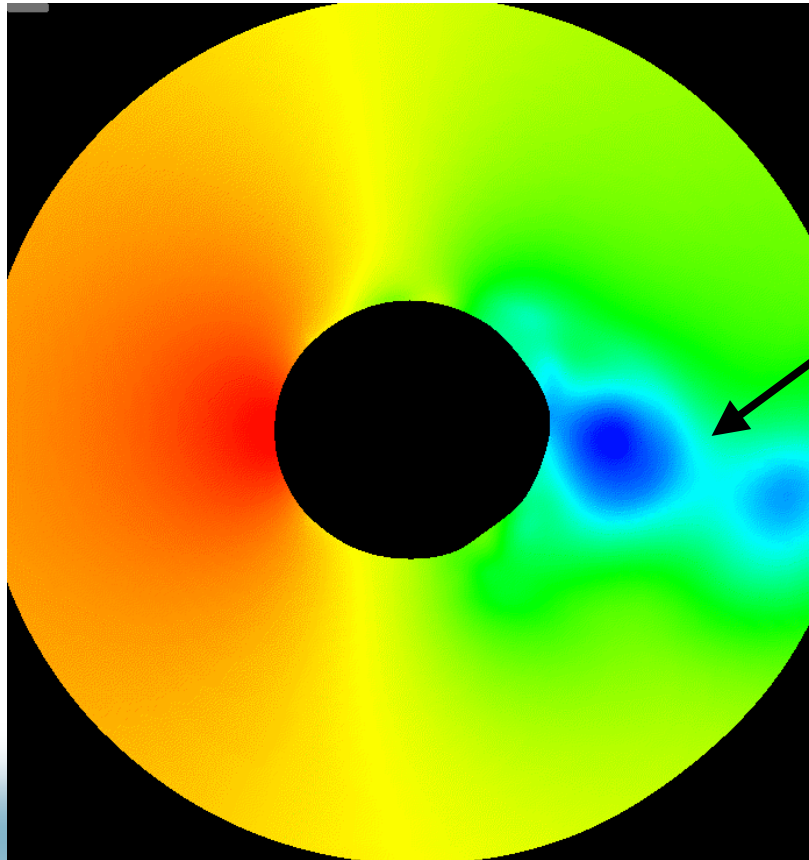
The amplitude at point a in case 2



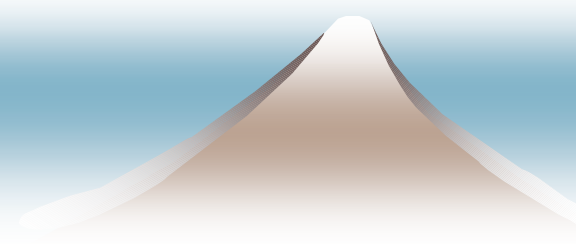
Deformation in case 2



Deformation in case 3



Karman vortex



Conclusion

- ◆ **We proposed the new scheme based on the loose coupling method for solving a CFS problem.**
- ◆ **The circular cylinder with elastic surface in uniform flow is chosen as the example. We indicate the satisfied results.**

